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Abstract: *We present a novel approach to automatic adaptivity in higher-order finite element methods (hp-FEM) which is free of analytical error estimates. A-posteriori error estimation is done via approximation pairs with different orders of accuracy, and the adaptivity is guided by discrepancies between global and local orthogonal projections. This approach is motivated by adaptive embedded higher-order methods for ODEs. We introduce a novel technique for hierarchic extension of polynomial spaces on higher-order finite elements. The adaptivity process yields a sequence of embedded stiffness matrices, which we solve efficiently using a novel combined direct-iterative algorithm. The methodology works in the same way for a wide range of PDE problems, and it works equally well for standard low-order FEM and for the hp-FEM. Numerical examples are presented.*

AMS subject classification: 65N30, 76M10

Keywords: Automatic adaptivity, higher-order finite elements, hp-FEM, hierarchic basis extension. embedded stiffness matrices.

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1 Introduction

The hp -FEM is a modern version of the finite element method capable of achieving extremely fast convergence rates by combining optimally finite elements of different sizes (h) and polynomial degrees (p) [1, 2, 3, 7, 8, 9, 10, 11, 12, 13, 14, 15]. The goal of our work is to develop adaptive hp -FEM algorithms with controlled accuracy in both space and time for complex multiphysics engineering problems. We face two major complications: First, extremely few analytical error estimates are available for arbitrary-order finite elements (not even in the context of linear elliptic problems), and second, extremely few analytical error estimates exist for multiphysics problems. Taking into account the tremendous mathematical difficulty of nonlinear time-dependent PDE systems describing some of these problems, a question is whether analytical error estimates for all problems of interest will ever be available.

During the last two decades, analytical error estimates have been derived mainly for single-physics problems solved by means of low-order methods (such as piecewise-linear FEM). Analytical error estimates differ a lot from one PDE to another, and are virtually impossible to combine into one universal methodology covering a wide range of multiphysics problems. Their practical application can be problematic, since sometimes they contain tuning parameters or dubious constants which need to be approximated using additional nontrivial mathematical tricks. The practitioner may not be skilled enough in mathematics or have enough time to do that. In the hp -FEM, an element can be refined in many different ways (typically around one hundred on 2D elements and several hundreds in 3D) [5, 12], and thus an elementwise-constant error estimate is not enough – one needs to know the *shape of the error* on every element, as a function.

In order to obtain a method which is applicable to a wide range of PDEs including multiphysics problems, and which works for both the standard FEM and the hp -FEM, we use an a-posteriori error estimate computed using *approximation pairs* (consisting of approximations with different orders of accuracy). The idea is analogous to embedded higher-order methods for ODEs [6]. The adaptive strategy is described in Section 2. A novel technique for hierarchic extension of polynomial spaces on arbitrary-order quadrilateral and triangular finite elements is described in Section 3. In Section 4 we introduce a novel technique for efficient solution of the sequence of embedded discrete problems obtained during the adaptivity proces. Section 5 uses a model problem to study the performance of the method.

2 PDE-Independent Adaptive Strategy

For the reasons explained above, we need to replace traditional analytical error estimates with a more universal approach working for a wide range of PDEs including multiphysics problems, as well as for the hp -FEM. We resort to an idea that has been used in the ODE community for a long time: In every time step, embedded adaptive higher-order ODE methods

compute efficiently two approximations with different orders of accuracy (an approximation pair). The error is estimated using their difference. If the difference is large, then the last step is repeated with smaller time step size, otherwise the time step size is increased. Of course, the PDE case is technically more complicated:

Initial step – construction of the approximation pair

In the initial step, we construct a pair of approximations with different orders of accuracy. We begin with a coarse mesh τ_0^c , and construct a reference mesh τ_0^r using global refinement of τ_0^c . This is done by increasing the polynomial degrees of all elements in the mesh τ_0^c by one and subdividing them uniformly in space, as illustrated in Fig. 1.

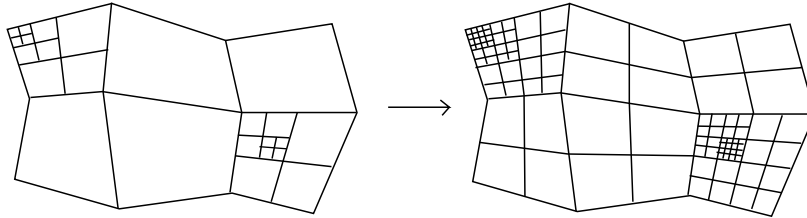


Figure 1: Coarse mesh τ_0^c and the globally refined reference mesh τ_0^r .

Next we build the stiffness matrix on the reference mesh τ_0^r , its LU factorization (using sophisticated multifrontal algorithms of the direct solver UMFPACK [4]), and solve on τ_0^r . By u_0^r let us denote the reference solution on τ_0^r . The initial algorithmic step is finished by projecting the reference solution u_0^r onto the coarse mesh τ_0^c . Note that an orthogonal projection yields the best approximation of u_0^r on the coarse mesh τ_0^c , and moreover, it is easier and faster to perform than to solve the finite element problem on the coarse mesh τ_0^c . The finite element problem is never solved on the coarse mesh. The multi-mesh *hp*-FEM [13] described above is used to perform efficiently all operations involving the coarse and reference meshes.

One step of the adaptive algorithm – update of the approximation pair

Let us set $k := 0$. The difference $e_k = u_k^r - u_k^c$ is used as an error function on the mesh τ_k^c . Note that such error estimator does not depend on the underlying equation and that it works without any limitations both for standard FEM and *hp*-FEM. If the global norm of the function e_k is less than a prescribed tolerance TOL , the computation stops. Otherwise, one marks for refinement elements in the coarse mesh τ_k^c with largest approximation error, until the number of newly added degrees of freedom (DOF) reaches a user-defined number N_{ref} . After performing these local refinements, one obtains a new coarse mesh τ_{k+1}^c . Analogous local refinements are done to the reference mesh τ_k^r so that the new reference mesh τ_{k+1}^r corresponds to a global refinement of the new coarse mesh τ_{k+1}^c . The finite element basis on

τ_k^r is extended hierarchically to a basis on τ_{k+1}^r (to be described in Section 3). Hence, the stiffness matrix S_k^r corresponding to the mesh τ_k^r is subset of the new stiffness matrix S_{k+1}^r on the mesh τ_{k+1}^r . This fact is used to optimize the solution of the discrete problem on the mesh τ_{k+1}^r (to be described in Section 4).

3 Hierarchic Basis Extensions on Higher-Order Elements

Let us consider a triangular element $K_{h,p}$ of degree $p \geq 1$. The corresponding polynomial space $P^p(K_{h,p})$ of dimension $(p+1)(p+2)/2$ contains 3 vertex functions associated with the vertices, $3(p-1)$ edge functions associated with the edges, and $(p-1)(p-2)/2$ bubble functions which are local to the element interior [12]. By the symbol $K_{h/2,p+1}$ let us denote the enriched element obtained by increasing the polynomial degree of $K_{h,p}$ by one and splitting it uniformly in space, as illustrated in Fig. 2.

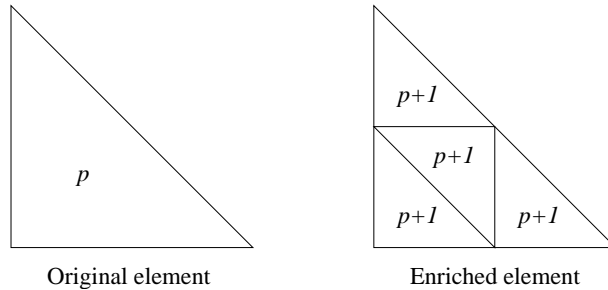


Figure 2: Triangular element $K_{h,p}$ and the corresponding enriched element $K_{h/2,p+1}$.

It is easy to calculate that the dimension of the enriched space on $K_{h/2,p+1}$ is $2p^2 + 7p + 6$: The standard hp -FEM basis on $K_{h/2,p+1}$ contains 6 vertex functions (one per vertex), $9p$ edge functions (p per edge) and $4p(p-1)/2$ bubble functions [$p(p-1)/2$ per subelement]. In order to create a new basis on $K_{h/2,p+1}$ containing the original basis on $K_{h,p}$ as a subset, let us begin with the $(p+1)(p+2)/2$ basis functions from $K_{h,p}$. Next we add 3 vertex functions associated with the new vertices (denoted by black dots in Fig. 3).

Next we add $p-1$ edge functions of degrees $2, 3, \dots, p$ to each of the six edges highlighted in Fig. 4. The set of edge functions is completed by adding one edge function of degree $p+1$ to each of the 9 edges of $K_{h/2,p+1}$. Next, we pick any three subelements (for example those highlighted in Fig. 5), and add to each of them $(p-1)(p-2)/2$ bubble functions of degrees $3, 4, \dots, p$. In a final step, we add $p-1$ bubble functions of degree $p+1$ to each of the four subelements.

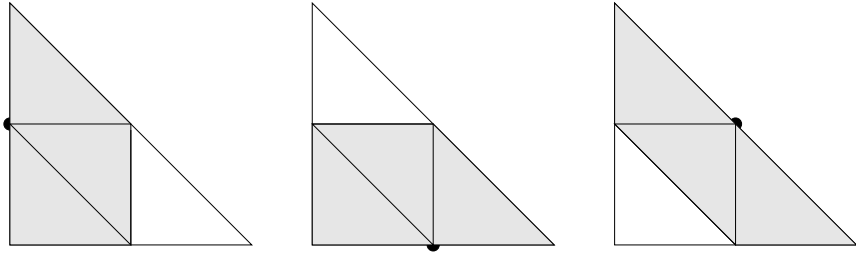


Figure 3: New vertex functions added to the basis of $K_{h/2,p+1}$.

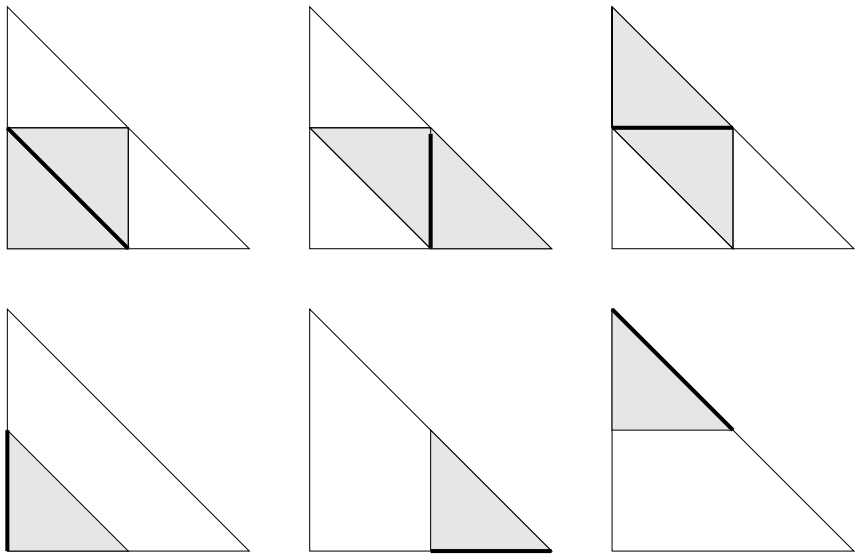


Figure 4: New edge functions of degrees $2, 3, \dots, p$ added to the basis of $K_{h/2,p+1}$.

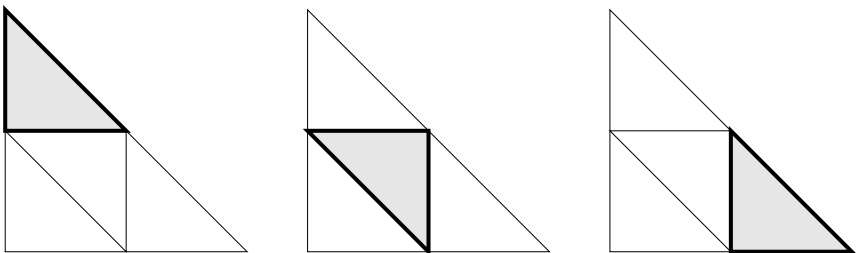


Figure 5: Three subelements to which we add bubble functions of degrees $3, 4, \dots, p$.

Proposition 3.1. *The $2p^2 + 7p + 6$ functions on $K_{h/2,p+1}$ defined above are linearly indepen-*

dent, and they generate the same piecewise-polynomial space as the standard hp -FEM basis on $K_{h/2,p+1}$.

The proof of this lemma is elementary – it is easy to check that the piecewise-polynomial spaces generated by the original and new basis are the same, that the number of basis elements in both cases is the same, and that the elements in the new basis are linearly independent.

Quadrilateral elements

The situation on quadrilaterals is even simpler than on triangles thanks to the product structure of the polynomial spaces. Consider two different directional polynomial degrees $p, q \geq 1$. A quadrilateral element $K_{h,p,q}$ and the corresponding enriched element $K_{h/2,p+1,q+1}$ are illustrated in Fig. 6.

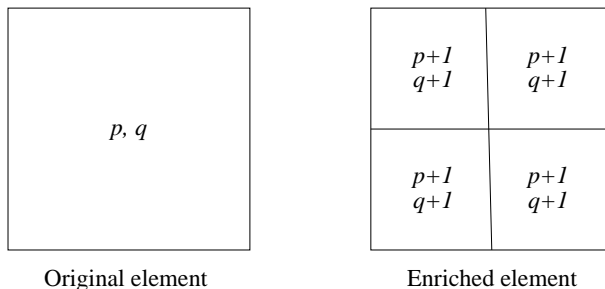


Figure 6: Quadrilateral element $K_{h,p,q}$ and the corresponding enriched element $K_{h/2,p+1,q+1}$.

Analogously to the triangular case, we calculate that the dimensions of the original and enriched spaces are $(p + 1)(q + 1)$ and $9 + 6p + 6q + 4pq = (2p + 3)(2q + 3)$, respectively. Due to the product character of the basis, it is sufficient to describe the extension of basis for a one-dimensional interval of degree p : The original basis has $p + 1$ elements (two vertex functions and $p - 1$ bubble functions). The enriched basis contains one additional vertex function associated with its midpoint, $p - 1$ additional bubble functions of degrees $2, 3, \dots, p$ (each being nonzero in one half of the interval only), and two additional bubble functions of degree $p + 1$ (each being nonzero in one half of the interval only). Thus the enriched space on the one-dimensional interval has dimension $(p + 1) + 1 + (p - 1) + 2 = 2p + 3$.

4 Solution of Embedded Discrete Problems

Thanks to the hierarchic extensions of finite element spaces during the adaptivity proces, the reference meshes $\tau_0^r, \tau_1^r, \tau_2^r, \dots$ yield a sequence of embedded stiffness matrices $S_0^r \subset S_1^r \subset S_2^r \subset \dots$. This fact can be used to optimize the solution of the discrete problem in every

adaptivity step. In this section, we describe two different methods that we designed for this purpose. Since our target applications are in multiphysics problems, both of them are based on direct sparse solvers. The performance of the methods will be compared in Section 5.

M1: Hierarchic extension of LU factorizations

During the initial step, we create the LU factorization of the stiffness matrix S_0^r corresponding to the initial reference mesh τ_0^r (more precisely, we use UMFPACK [4] for this purpose). In every other adaptivity step, the LU factorization from the previous step is extended by adding new columns and rows corresponding to the newly added basis functions, as illustrated in Fig. 7.

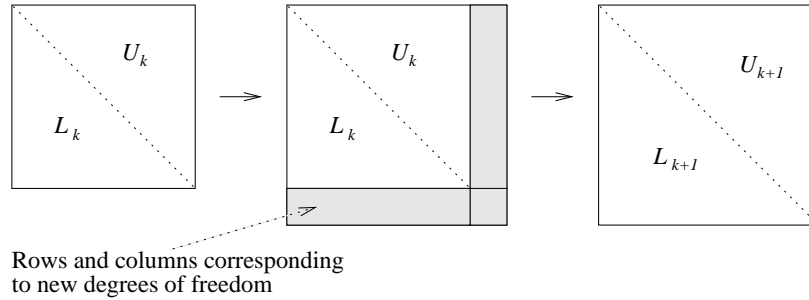


Figure 7: Extension of the LU factorization of the stiffness matrix $S_k^r = L_k U_k$ to the LU factorization $S_{k+1}^r = L_{k+1} U_{k+1}$ corresponding to the next reference mesh τ_{k+1}^r .

The algorithm is easy to design as it only involves elementary matrix operations. With the LU factorization of the new stiffness matrix S_{k+1}^r in hand, the new reference solution u_{k+1}^r is computed instantly. By projecting the new reference solution on the mesh τ_{k+1}^c , we obtain its best representant u_{k+1}^c on τ_{k+1}^c and thus also the new error function $e_{k+1} = u_{k+1}^r - u_{k+1}^c$. Hence, one step of the adaptivity algorithm is completed.

M2: Combined direct-iterative method

The first discrete problem on the initial reference mesh τ_0^r has the form $S_0^r Y_0 = F_0$. We solve it via UMFPACK and keep the LU factorization of S_0^r . After the first mesh refinement, we obtain a new mesh τ_1^r . Due to the hierarchic extension of the finite element space, the corresponding stiffness matrix S_1^r consists of four blocks S_0^r , B_1 , C_1 and S_1 . The right-hand side of the new discrete problem consists of the original vector F_0 and a new vector F_1 corresponding to the newly added basis functions. The situation looks as follows:

$$\begin{pmatrix} S_0^r & C_{1,1} \\ B_{1,1} & S_1 \end{pmatrix} Y = \begin{pmatrix} F_0 \\ F_1 \end{pmatrix}. \tag{1}$$

We can assume that the matrix S_1 is nonsingular since it corresponds to the solution of the original PDE problem in a subdomain equipped with homogeneous essential boundary conditions. We employ UMFPAK to construct the LU factorization of the matrix S_1 and solve efficiently the system $S_1 Y_1 = F_1$. The solution of the system (1) can be written in the form

$$Y = \begin{pmatrix} Y_0 + \Delta Y_0 \\ Y_1 + \Delta Y_1 \end{pmatrix}. \quad (2)$$

By substituting (2) into (1), we obtain

$$\begin{aligned} S_0^r Y_0 + S_0^r \Delta Y_0 + C_{1,1} Y_1 + C_{1,1} \Delta Y_1 &= F_0, \\ B_{1,1} Y_0 + B_{1,1} \Delta Y_0 + S_1 Y_1 + S_1 \Delta Y_1 &= F_1. \end{aligned} \quad (3)$$

Application of $S_0^r Y_0 = F_0$ and $S_1 Y_1 = F_1$ simplifies this to

$$\begin{aligned} S_0^r \Delta Y_0 + C_{1,1} Y_1 + C_{1,1} \Delta Y_1 &= 0, \\ B_{1,1} Y_0 + B_{1,1} \Delta Y_0 + S_1 \Delta Y_1 &= 0. \end{aligned} \quad (4)$$

The unknown vectors ΔY_0 and ΔY_1 are computed using the following iterative method:

$$\begin{aligned} S_0^r \Delta Y_0^{(k+1)} &= -C_{1,1} Y_1 - C_{1,1} \Delta Y_1^{(k)}, \\ S_1 \Delta Y_1^{(k+1)} &= -B_{1,1} Y_0 - B_{1,1} \Delta Y_0^{(k)}, \end{aligned} \quad (5)$$

which starts with $\Delta Y_0^{(0)} = 0$ and $\Delta Y_1^{(0)} = 0$. When this process converges, we know the solution u_1^r on the mesh τ_1^r .

After n refinement steps, the discrete problem has the form

$$\begin{pmatrix} S_0^r & C_{1,1} & C_{1,2} & \dots & C_{1,n} \\ B_{1,1} & S_1 & C_{2,2} & \dots & C_{2,n} \\ B_{1,2} & B_{2,2} & S_2 & \dots & C_{3,n} \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ B_{1,n} & B_{2,n} & B_{3,n} & \dots & S_n \end{pmatrix} \begin{pmatrix} \bar{Y}_0 + \Delta Y_{0,n} \\ \bar{Y}_1 + \Delta Y_{1,n} \\ \bar{Y}_2 + \Delta Y_{2,n} \\ \vdots \\ \bar{Y}_n + \Delta Y_{n,n} \end{pmatrix} = \begin{pmatrix} F_0 \\ F_1 \\ F_2 \\ \vdots \\ F_n \end{pmatrix}. \quad (6)$$

Here, $\bar{Y}_j = Y_j + \sum_{k=j}^{n-1} \Delta Y_{j,k}$, $j = 0, 1, \dots, n$. The $(j+1)$ th equation in the system (6) has the form

$$\sum_{k=1}^j B_{k,j}(\bar{Y}_{k-1} + \Delta Y_{k-1,n}) + S_j(\bar{Y}_j + \Delta Y_{j,n}) + \sum_{k=j+1}^n C_{j+1,k}(\bar{Y}_k + \Delta Y_{k,n}) = F_j. \quad (7)$$

The vector $(\bar{Y}_0, \bar{Y}_1, \dots, \bar{Y}_{n-1})^T$ is the solution of the system obtained after $n-1$ refinement steps. In other words,

$$\sum_{k=1}^j B_{k,j} \bar{Y}_{k-1} + S_j \bar{Y}_j + \sum_{k=j+1}^{n-1} C_{j+1,k} \bar{Y}_k = F_j, \quad j = 0, 1, \dots, n-1. \quad (8)$$

Substituting this along with $S_n Y_n = F_n$ into (7), and using the fact that $\bar{Y}_n = Y_n$, we obtain

$$\begin{aligned} \sum_{k=1}^j B_{k,j} \Delta Y_{k-1,n} + S_j \Delta Y_{j,n} + C_{j+1,n} Y_n + \sum_{k=j+1}^n C_{j+1,k} \Delta Y_{k,n} &= 0, \quad j = 0, 1, \dots, n-1, \\ \sum_{k=1}^n B_{k,n}(\bar{Y}_{k-1} + \Delta Y_{k-1,n}) + S_n \Delta Y_{n,n} &= 0. \end{aligned} \quad (9)$$

The unknown vectors $\Delta Y_{0,n}, \Delta Y_{1,n}, \dots, \Delta Y_{n,n}$ are computed using the following iterative method:

$$\begin{aligned} S_j \Delta Y_{j,n}^{(k+1)} &= - \sum_{k=1}^j B_{k,j} \Delta Y_{k-1,n}^{(k)} - C_{j+1,n} Y_n - \sum_{k=j+1}^n C_{j+1,k} \Delta Y_{k,n}^{(k)}, \quad j = 0, 1, \dots, n-1, \\ S_n \Delta Y_{n,n}^{(k+1)} &= - \sum_{k=1}^n B_{k,n}(\bar{Y}_{k-1} + \Delta Y_{k-1,n}^{(k)}). \end{aligned} \quad (10)$$

After n th refinement step, we only construct and store the LU factorization of one relatively small matrix S_n . The above iterative process for the computation of u_n^r is based on the solution of n linear systems with the matrices S_0^r, S_1, \dots, S_n whose LU factorizations are known. Our preliminary results show that this iteration converges very fast both for symmetric positive definite matrices and for large ill-conditioned matrices. The convergence analysis is in progress.

5 Numerical Example

Let us illustrate the methodology on a plane-strain model problem of linear elasticity describing the elastic behavior of a long hollow workpiece subject to vertical loading on its top surface. The workpiece lies on a rigid surface, as shown in Fig. 8.

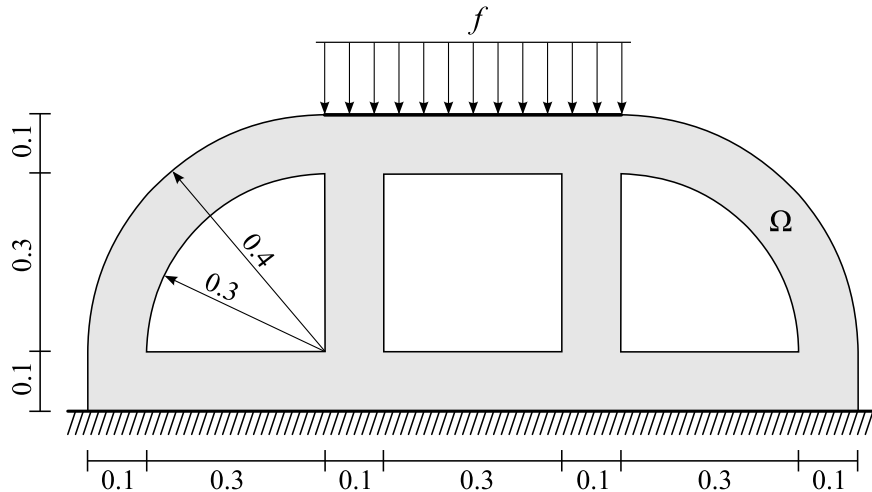


Figure 8: Computational domain.

Fig. 9 shows the resulting stress distribution. Piecewise-linear mesh and hp -FEM mesh corresponding to roughly the same relative error 0.5% are shown in Figs. 10 and 11, respectively. Convergence histories of standard FEM and hp -FEM in energy norm are compared in Fig. 12. Notice that the hp -FEM converges exponentially.

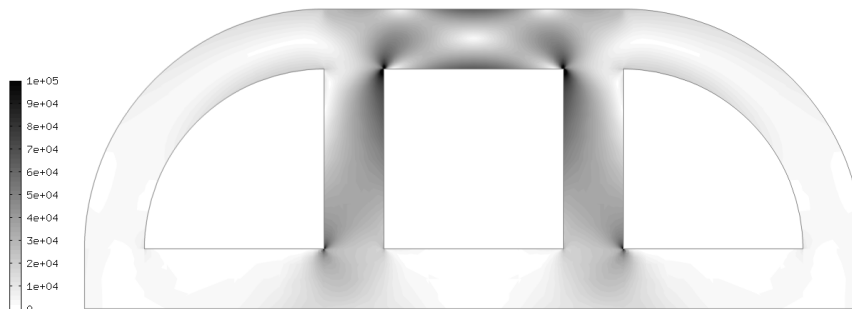


Figure 9: Stress distribution.

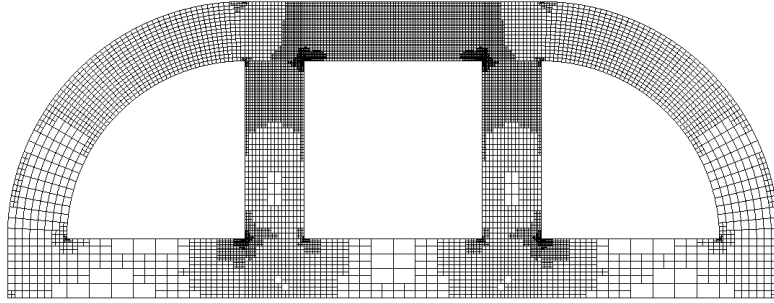


Figure 10: Mesh consisting of lowest-order elements (approx. error 0.5% and 21000 DOF).

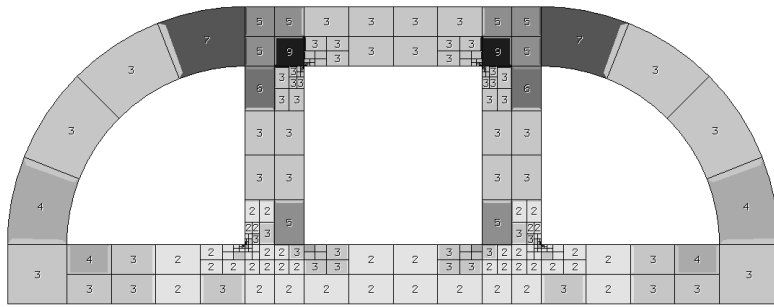


Figure 11: Mesh consisting of higher-order elements (approx. error 0.5% and 2500 DOF).

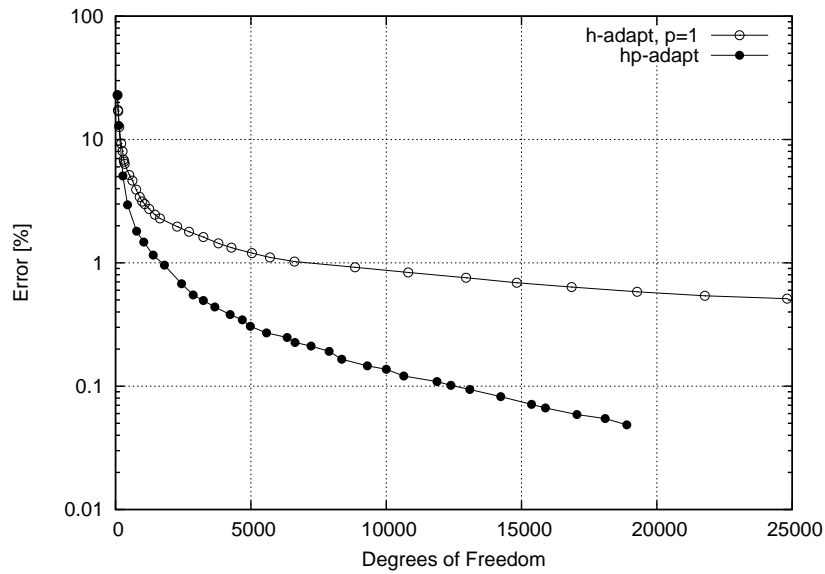


Figure 12: Convergence comparison.

Performance of method M1

First we show that (quite surprisingly to us) the technique M1 from Section 4 is not very suitable for practical use. To illustrate this, it is sufficient to consider a relatively small reference mesh τ_0^r with 16129 DOF. UMFPACK is used to compute the LU factorization of the corresponding stiffness matrix S_0^r . We refine the mesh τ_0^r by adding 100, 1001, 2500, 5002 and 10002 DOF, respectively (i.e., the new reference mesh τ_1^r has 16139, 17130, 18629, 21131 and 26131 DOF). Table 1 shows the CPU times needed by UMFPACK to compute the LU factorization of the corresponding stiffness matrix S_1^r from scratch as well as the CPU time needed to construct the LU factorization of S_1^r by extending the LU factorization of the stiffness matrix S_0^r , using the method M1.

$\text{rank}(S_0^r)$	DOF added	$\text{rank}(S_1^r)$	UMFPACK time (ms)	M1-time (ms)
16129	100	16139	479	411
16129	1001	17130	545	4212
16129	2500	18629	640	11403
16129	5002	21131	720	24515
16129	10002	26131	1327	58637

Table 1: Performance of the method M1.

The reader can see that the method M1 is only useful when very small number of new DOF is added, and it does not scale well when this number is increased.

Performance of method M2

To illustrate the performance of the method M2, let us consider two different reference meshes τ_0^r with 130305 and 261121 DOF, respectively. For each of them, we construct five different reference meshes τ_1^r by adding 1001, 2500, 5002 and 10002 DOF, respectively. Tables 2 and 3 show the CPU times needed by UMFPACK to construct the LU factorization of the stiffness matrix S_1^r in all cases, along with the CPU time needed by our method M2 to obtain the solution u_1^r on the mesh τ_1^r (using the existing LU factorization of S_0^r). The iterative method M2 stops when the l^2 -norm of the residuum is less than *eps*.

These results are encouraging, and another obvious advantage of the method M2 is that it can handle very large matrices including those which no longer can be LU-factorized. The method needs to be further studied and optimized, and applied to indefinite matrices arising in complex multiphysics problems. Our preliminary results indicate that the method converges very well also for strongly ill-conditioned indefinite matrices. Convergence of the

rank(S_0^r)	DOF added	rank(S_1^r)	UMFPACK time (ms)	M2-time (ms) $eps = 10^{-2}$	M2-time (ms) $eps = 10^{-4}$	M2-time (ms) $eps = 10^{-6}$
130305	1001	131306	4454	633	1750	3241
130305	2500	132805	4156	648	1809	3316
130305	5002	135307	4327	768	1874	3487
130305	10002	140307	4420	863	2008	3631

Table 2: Performance of the method M2, rank(S_0^r) = 130305.

rank(S_0^r)	DOF added	rank(S_1^r)	UMFPACK time (ms)	M2-time (ms) $eps = 10^{-2}$	M2-time (ms) $eps = 10^{-4}$	M2-time (ms) $eps = 10^{-6}$
261121	1001	262132	11300	1262	2646	4133
261121	2500	263621	10355	1257	2771	4346
261121	5002	266123	10418	1301	2810	4370
261121	10002	271123	11432	1792	3077	4536

Table 3: Performance of the method M2, rank(S_0^r) = 261121.

iterative proces needs to be analysed, as wel as the influence of the parameter eps in the stopping criterion. The residual stopping criterion needs to be replaced with a more realistic convergence criterion based on the H^1 -norm in the finite element space. We hope to report on our progres soon.

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